ABSTRACT

This paper explores the design space that exists between multi blade, high-solidity water-pumping turbines with trapezoidal blade design and modern rectangular horizontal axis wind turbines (HAWTs). In particular, it compares the features and performance of a small 18-bladed, high-solidity HAWT with trapezoidal blade to that of a rectangular bladed 18-bladed HAWT. This is achieved through a Modal analysis on the exist trapezoidal blade and optimize rectangular blade along with dynamic response analysis of blade in ANSYS software. The model of blade was developed in CATIA. Dynamic analysis was performed for the blade by using the finite element method.

Keywords—Blade Design, optimization; modeling; finite element analysis

I. INTRODUCTION

Blade is the key component to capture wind energy. It plays a vital role in the whole wind turbine. In this paper, design and analysis are conducted with layered shell elements to treat a horizontal axis 18-blade wind turbine based on ANSYS. The paper studied about the design of exist wind mill located at Pusad and compare the performance and life of blade with optimize design on basis of Modal and dynamic analysis. The optimization of blade is carried out by considering parameter like shapes of blade profile, stresses, deflection and buckling on blade.

Referring to data of exist wind mill blade provide by wind turbine company, parameters of the blade were given as follows:
Design wind speed \( V = 7 \text{ m/s} \), rotor diameter \( D = 3 \text{ m} \), blade number \( B = 18 \). Tip speed ratio range of Low-speed wind turbines, \( \lambda = 1.6 \)

Optimum angle of attack 30°

According Design data book the applied Lift coefficient=1.3, Drag coefficient=0.1.

Lift Force on Blade=14.82 N
Drag Force on Blade=1.1403 N

<table>
<thead>
<tr>
<th>Sr. No.</th>
<th>Parameters</th>
<th>Specification</th>
</tr>
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<tbody>
<tr>
<td>1</td>
<td>No. of Blade</td>
<td>18 Nos.</td>
</tr>
<tr>
<td>2</td>
<td>Blade Materials</td>
<td>Galvanized Iron</td>
</tr>
<tr>
<td>3</td>
<td>Size of Blade (Trapezoidal Shape)</td>
<td>920×440×195mm</td>
</tr>
<tr>
<td>4</td>
<td>Area of Blade</td>
<td>0.291 m²</td>
</tr>
<tr>
<td>5</td>
<td>Thickness of Blade</td>
<td>1mm</td>
</tr>
<tr>
<td>6</td>
<td>Angle of Attack of Blade</td>
<td>30°</td>
</tr>
<tr>
<td>7</td>
<td>Rotor Diameter</td>
<td>3 meter</td>
</tr>
</tbody>
</table>

Table: 1Technical Specification of Blade

II. MODELING OF EXIST BLADE DESIGN

(Rectangular Shape)

Fig: 2.1 Model of Blade

Fig: 2.2 Models of Blade & Rotor
III. DYNAMIC FINITE ELEMENT ANALYSIS OF THE EXIST BLADE

Dynamic finite element analysis of the blade mainly refers to the vibration modal analysis using the finite element theory. Modal analysis is used to identify natural frequencies, especially low-order frequencies and vibration modes of wind turbine blades. From the modal we can learn in which frequency range the blade will be more sensitive to vibrate. Blades should be designed to avoid the resonance region with the tower and other components in order to prevent some destruction of related components. In this paper, the finite model of the blade has been established in ANSYS by importing the blade surface model created previously combined with the actual layer structure of the existing blades. Modal analysis was carried out to check whether the mechanical properties of the blade meet certain safety requirements.

a. Finite Element Modeling

The finite element analysis of blade is carried out in ANSYS software. The design of blade imported from CATIA software which was analyzed in ANSYS.

The shell unit shell 63 was chosen to simulate structure of blade. The material properties were approximately defined as isotropic, as the blade was made of galvanized iron materials. The material number and properties were defined by the Material Models menu. The corresponding real constants were distributed to every part of the blade and appropriate grid size was set. All the areas were meshed by MASHTOOL in the way of Free Mesh. The created FEM model of the blade consisted of 810 elements, 776 nodes (Fig. 3.1) shows the lamination attribute of one selected element.

Fig: 3.1 FEM blade model

b. Modal Analysis of Blade

There are many ways for ANSYS modal analysis, of which the Block Lanczos method is most widely used because of its powerful features. Moreover, it is frequently applied with model of solid units or shell units that is why this paper chose Block Lanczos to perform the modal analysis. The vibration modes of the first five orders were extracted with the frequency range of 0-9999Hz. The connections of blades and rotor could be regarded as fixed, so it is only need to restrict all DOFs of the root, for modal analysis does not require applying loads. At last, after solving with the solver, the vibration modes of all the orders (Fig. 3.2) and the result of frequencies (Table 1) could be observed in the post-processor.
IV. OPTIMIZATION OF EXIST BLADE DESIGN

The optimization of exist blade design is carried out on basis of different parameters like shape profile of blade, Maximum Stresses and deflection on blade surface. These parameters are very important for consideration. The design of Wind Mill Rotor is design such that its pumped 1800 Liters of Water per day.

a. Annual Energy consumption per Year

The energy required to pumped 1800 Liters water from a well of depth about 25 m is about 120 Watts per Day approximately.

Total annual energy consumption = Energy consumption per hour × Total annual hours

Total annual energy consumption = 120×8760 =1051.200 kwh

But this is the energy when wind will flow at rated wind speed throughout the year, which is never a case. Therefore in order to get realistic energy output, we have to multiply the above numbers by the capacity factor. For wind energy capacity factor is assumed to be 30 %.) [11]

Annual Energy Production = 120×8760×0.3

= 315.360 kwh

Estimation of the annual energy output of a wind machine using capacity factor is an approximate method for finding annual output. For more accurate analysis, one should know long term wind distribution.

b. Estimation of Required Windmill Power Rating

The total energy annual requirement is 1100 kwh. Then what should be the size of wind turbine that is required to be installed to meet the energy requirement.

Annual Energy Requirement =1100kwh

Coefficient of Performance = 0.40

Wind Speed at Height of 15 meter = 7m/s

Density of air = 1.22 kg/m³

Capacity Factor = 0.30 (30% of the time, wind machine is producing energy at rated power)

No. of Hours in Year = 8760 Hours

c. Calculation of Power Density of Wind (Power per unit Area)

Ideal Power density of air

\[ P = \frac{1}{2} \times \rho \times V^3 \]

= 0.5×1.22×(7×7×7) = 171.5 w/m²

Actual power density that will be converted to useful energy

= coefficient of performance× other losses

By considering

Other losses = 0.324

Actual power density = 171.5×0.324

= 55.55 w/m²

Annual energy density (useful)

= power density× no of hours per Year

= 55.55×8760

= 486.75 kwh/m²

By considering the capacity factor (30%)

Real annual energy density

= Annual energy density (useful) × capacity factor

= 486.75×0.30

=146.02 kwh/m²

d. Calculation of Rotor (Blade) Size

Area of the rotor = Total annual energy required / Real annual energy density

= 1051.200 / 146.02

= 7.199 m²

e. Radius of Rotor (R)

\[ A = \pi R^2 \]

\[ 7.199 = \pi R^2 \]

R = 1.514 m

Diameter of Rotor =3 m

f. Power Rating of Windmill

= Actual power density × Area of Rotor

= 55.55 × 7.199

=399.904 watts

V. MODELING OF OPTIMIZE BLADE DESIGN

In this section the modeling of optimizes blade design is carried out on basis of calculated data in CATIA modeling software.

The blade is having size of 920×400mm with optimum incident angle of 30°.
VI. DYNAMIC FINITE ELEMENT ANALYSIS OF THE OPTIMIZE BLADE

The modal which has been created in CATIA modeling software imported in ANSYS and treated that blade shape as SHELL 63 element and the dynamics analysis was carried out. Modal analysis was carried out to check whether the mechanical properties of the new blade design meet certain safety requirements. The created FEM model of the blade consisted of 710 elements, 715 nodes (Fig. 5 (a)) shows the lamination attribute of one selected element.

Fig: 4.2 Modal of Blade with rotor assembly

Fig: 4.3 Meshing of Optimize Blade design

Fig: 4.4 First Five modes of Vibrations

Table 2. Frequencies of the first five orders

<table>
<thead>
<tr>
<th>Mode orders</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
</tr>
</thead>
<tbody>
<tr>
<td>Frequencies</td>
<td>117.9</td>
<td>279.09</td>
<td>555.36</td>
<td>675.36</td>
<td>728.14</td>
</tr>
</tbody>
</table>

VII. RESULTS & DISCUSSION

From Modal analysis carried out on exist and optimize blade it is found that the dynamic response for new rectangular blade is improved rather than exist design. The maximum resonance frequency of exist blade (Trapezoidal Shape) design is about 650Hz, whichhas to be improved up to 720Hz in new blade design (Rectangular Shape).

VIII. CONCLUSION
This paper applied to realize the aerodynamic contour optimization design of wind turbine blade. The way of combining CATIA and ANSYS was adopted to establish the blade model so as to describe actual shape and layer structure of the blade precisely. The dynamic performance of the exist blade (Trapezoidal Shape) and new blade (Rectangular Shape) was checked by modal analysis, providing a reference for structure design and other analyses.

REFERENCES